

MICROCOLUMN FOR EXTRACTION OF ANALYTES
FROM LIQUIDS

RELATED APPLICATION

5 This application is a continuation-in-part of
U.S. Patent Application Serial No. 08/275,781 filed July
15, 1994, which is incorporated herein by reference.

BACKGROUND

10 The present invention relates to microcolumns
for extraction of an analyte from a liquid sample, and
particularly extraction of an analyte from biological
fluids.

 Accurate and inexpensive detection of analytes
15 present in liquid samples, for example in biological
fluids, such as blood and urine, is important to health
care. Tests for analytes in blood and urine are
conducted to monitor the health of patients, detect the
presence of disease conditions, and monitor for the use
20 of illegal or restricted drugs. For example, doctors,
when administering drugs such as antiarrhythmics,
asthmatic drugs, insulin, and anticoagulants, check the
drug content of the blood to regulate the dosages of the
patient. Drugs that can be abused, such as heroin,
25 marijuana, cocaine, and codeine, can be tested to
determine abuse of the drug, such as by employees and by
athletes.

 A technique used for detection of analytes
includes selectively extracting the analyte from the
30 biological fluid onto a solid media. The analyte is then
removed from the solid media by a suitable elution
liquid, and tests are conducted to determine whether the
analyte is present in the eluent liquid, such as by gas
or liquid chromatography.

35 Prior art extraction columns have been
effectively used. For example, it is known to use
particulate silica as the solid media in a column. In

addition, silica has been provided embedded within an inert matrix of polytetrafluoroethylene ("PTFE") in the form of an extraction disk, which can be preloaded in a plastic barrel.

A problem with use of PTFE to hold the silica is that PTFE is hydrophobic and can require pre-conditioning with alcohol and high pressure so that the aqueous sample can flow therethrough. This increases the time and manpower required for the analysis.

Although these prior art devices can be effective, it is desirable to improve on these devices. It is desirable that the extraction device be fast, remove a high percentage of the analyte from the sample, be transportable, storable without damage, and be inexpensive. Moreover, it is desirable that any such device be compatible with existing automated equipment, and not leach into the biological fluid or the eluent liquid, any compound that could interfere with the analytical results.

Moreover, it is desirable to minimize the volume of biological fluid and wash eluent liquid. By minimizing the liquid volume, a more concentrated sample is obtained for analysis, the sensitivity of the test is enhanced, and less biological fluid needs to be obtained from the subject. High yields from the biological fluid with minimum elution volumes can be obtained by maintaining uniform flow through the extraction media, with no channeling and no dead volume.

SUMMARY

The present invention is directed to an extraction apparatus that meets these needs. The apparatus is useful for extracting a substance (also referred to as an analyte) from a liquid sample. The apparatus comprises a container, typically a microcolumn, having an entrance, an opposed exit, and a passage therebetween for passage of a liquid sample containing an

analyte therethrough. Within the passage is a thin layer of a microparticulate extraction media, typically silica particles. The media is selected for extracting the analyte from the liquid sample. The extraction media has a small particle size of less than 20 microns, which is provided in a very thin layer, so that the ratio of the effective diameter of the extraction media layer to the thickness of the layer is at least 5, and preferably at least 10.

The extraction media is sandwiched between upper and lower compression layers, which compress the silica extraction media therebetween. The compression layers are sufficiently porous that the liquid sample can flow therethrough, and are formed from a flexible, hydrophilic material. This is in contrast to the prior art preformed disks, which are made of polytetrafluoroethylene, which is hydrophobic, and thus slows down the flow of sample through the extraction media and utilizes preconditioning. The compression layer has a pore size less than the particle size of the extraction media, and is preferably formed of a spongy, glass fiber, having no binder.

Preferably the microcolumn also includes an upper mesh flow distributor above the upper compression layer, and a lower mesh flow distributor below the lower compression layer, sandwiching the compression layers and the layer of extraction media therebetween. The flow distributors hold the extraction media and the compression layers in the microcolumn and help distribute flow of the liquid sample to avoid channeling.

In a preferred version of the invention, the bottom of the container is substantially flat, with the exit substantially centrally located in the bottom. This ensures uniform flow of the liquid sample through the container.

Due to the combination of the very thin layer of extraction media and the compression layers, rapid

extraction of an analyte from a biological fluid can be obtained, with very small volumes of biological fluid, i.e., less than 0.5 ml, and only very small samples of elution liquid are needed, on the order of 0.5 to 0.75 ml. In addition, the extraction device of the present invention is inexpensive to use and manufacture, is stable during storage and transportation, and is compatible with existing automated equipment.

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DRAWINGS

These and other features, aspects, and advantages of the present invention can be better understood with reference to the following description, appended claims, and accompanying drawings, where:

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FIG. 1 is a perspective view of one version of a microcolumn according to the present invention;

FIG. 2 is a side elevation view, exploded, partly in section, of region 2 of the microcolumn of FIG. 1;

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FIG. 3 is a side elevation view, partly in section, of the microcolumn of FIG. 1 in region 2 of FIG. 1;

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FIG. 4 is a side elevation view, partly in section, of a different version of a microcolumn according to the present invention; and

FIG. 5 is a top plan view of the microcolumn of FIG. 4.

DESCRIPTION

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An apparatus 10 for extracting an analyte from a liquid sample is shown in FIGS. 1-3. The apparatus 10 comprises a microcolumn 12, which serves as a container for an extraction sandwich system. The extraction system is comprised of a five-layer sandwich construction, that includes (i) a thin extraction layer 14 of microparticulate solid extraction medium, (ii) an upper flow distributor 16a, (iii) a lower flow distributor 16b,

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and two compression layers, (iv) an upper compression layer 18a between the upper flow distributor 16a and the extraction layer 14, and (v) a lower compression layer 18b between the lower flow distributor 16b and the extraction layer 14.

The microcolumn 12 has generally a tubular configuration, and has an entrance 20, an opposed exit 22, and a passage 23 therebetween for generally vertical flow. The flow can be effected with a vacuum system (not shown) or gravity alone. The passage 23, which is also referred to as a central bore, contains the extraction system. The exit 22 is preferably in the form of a luer-lock, which allows the apparatus 10 to be used with conventional automated extraction apparatus, such as a vacuum extraction apparatus, which are designed to receive an extraction column having a luer-lock.

A liquid sample flows in the direction of arrow 26 shown in FIG. 2 through the passage 23.

The portion of the microcolumn 12 above the extraction sandwich system serves as a reservoir for the liquid sample, from which an analyte is to be extracted, and also a reservoir for an eluent liquid.

All of the components of the apparatus 10 are made of materials that are substantially inert to biological fluids so that when blood or urine is passed through the apparatus 10, substantially nothing passes from the apparatus 10 into the blood or urine. Preferably, the microcolumn 12 is made of polypropylene, or alternatively, a fluorinated polymer.

A typical microcolumn according to the present invention has an internal diameter of about 1/4 to 1 inch, and a length, excluding the luer tip, of about 2 to about 6 inches.

The microcolumn 12 need not have the shape shown in the figures. For example, it need not be cylindrical in horizontal cross-section. In addition, in one embodiment of the invention, the entrance 20 can be

designed to receive a luer-lock extension so that a reservoir containing a liquid sample can be piggybacked on top of the microcolumn 12.

5 The extraction media 14 is formed of silica, such as a silica gel, constituted pure glass, modified silica, or polymeric resin such as divinyl benzene. The media particles are of small particle size, preferably having a number average of particle size of less than 20 microns, and more preferably, less than 10 microns. A
10 suitable silica extraction media is described in U.S. Patent No. 4,650,714, which is incorporated herein by reference. A preferred microparticulate silica extraction media is available from J.T. Baker Chemical Company of Phillipsburg, New Jersey, and is sold under
15 their catalog number 7049-01.

Because of the small particle size of the silica, and because it is not impregnated into a hydrophobic layer such as polytetrafluoroethylene, it is possible to have a very thin extraction layer.
20 Typically, the thickness of the extraction layer is less than 1 mm, and typically from about 0.1 to about 0.8 mm. Preferably, the ratio of the effective diameter of the extraction layer to the thickness of the extraction layer is at least 5, more preferably at least 10, and most
25 preferably at least 15. By "effective diameter" there is meant:

$$D_{eq} = (4A/\pi)^{1/2}$$

30 where D_{eq} is the equivalent diameter and A is the cross-sectional surface area of the bore of the microcolumn 12.

Preferably, the silica extraction media is placed in the microcolumn 12 using a slurry packing technique, utilizing as the carrier isopropanol.

35 The chief purpose of the compression layers 18 is to hold the extraction media in place and compressed as a thin extraction layer. Accordingly, the compression

layers 18 have a pore size less than the particle size of the silica extraction media. They are sufficiently porous that the liquid sample can flow therethrough, and are composed of a flexible, hydrophilic material.

5 Preferably the compression layers 18 are resilient or "spongy" to hold the microparticles in place. A preferred pore size for the compression layers is less than 5 microns, and more preferably less than 3 microns. The compression layers 18 generally are of the same
10 thickness, having a thickness typically of from about 1/4 to about 1 mm, and preferably about 1/2 mm.

A suitable compression layer comprises a glass microfiber media made of analytically clean material. Suitable materials, which are available from Whatman
15 Specialty Products, Inc. of Fairfield, New Jersey, include a borosilicate glass fibers that are analytically clean and include no binder. This material, when purchased, has a smooth side and a rough side, where the smooth side is of lower porosity than the rough side.
20 Preferably, it is the smooth side that is placed in contact with the microparticles of the extraction layer 14.

The flow distributors 16, which are formed of a flexible mesh material, help provide uniform flow of the
25 sample through the column, and physically retain the compression layers and microparticulate material in place in the column. Preferably, the mesh is 200 mesh or smaller (i.e., has a mesh number of 200 or higher). It is made of polypropylene, or alternatively,
30 polytetrafluoroethylene. A suitable material is available from Tetko, Inc. of Briarcliff Manor, New York, under catalog number 5-420134.

As shown in FIG. 3, the lower flow distributor 16b seats against the sloped bottom portion of the
35 microcolumn. The upper flow distributor 16a is sized so that it is held in the bore of the microcolumn 12 by a compression fit.

As described, the apparatus 10 is easy and inexpensive to manufacture, is transportable, and efficiently and effectively removes analytes from liquid samples, requiring only small amounts of the liquid sample and small amounts of eluent fluid. The microcolumn can easily be injected molded.

FIG. 4 shows an apparatus 40 that is substantially the same as the apparatus 10 of FIG. 1, except the configuration of container 42 of apparatus 40 is different from the configuration of container 12 of FIG. 1. In particular, apparatus 40 uses the same type of extraction layer 14, upper and lower flow distributors 16a and 16b, and upper and lower compression layers 18a and 18b as does apparatus 10. The container 42 has an open entrance or top 44, a peripheral side wall 46, and a bottom 48. The peripheral side wall 46 is generally circular in horizontal section. The internal wall or surface 50 of the bottom 48 is substantially flat, and is substantially perpendicular to the vertical fluid flow path through the apparatus 40. There is an exit hole 51 through the bottom 48 that communicates with an exit passage 52. A liquid sample is poured through the top of entrance 44, and passes through exit hole 51 and through passage 52. The exit hole 51 and passage 52 are substantially centrally located in the middle of the bottom 48. Preferably the exit hole 51 is the configuration of an inverted truncated cone, to direct liquid flow into the passage 52.

The flow pattern, as a result of the flat inner surface 50 and its centrally located exit 51, is axially located through the extraction layer 14 without channeling, i.e., substantially the entire microparticulate layer is used for extraction. This results in homogenous absorption of compounds of interest in the extraction layer 14, and efficient transmission of liquid through the system with minimum entrapment of liquid. Furthermore, in this design, due to the porosity

of the glass mat and the polypropylene screen flow distributors 16, the apparatus has low internal volume with minimal liquid retention. Minimum liquid retention reduces the amount of solvent used to remove any substances retained by the extraction medium. Thus, the apparatus 40 provides maximum extraction efficiency by the extraction medium, yet minimum solvent usage to reclaim the absorbed compounds of interest from the sorbent layer.

It is also an important feature of the present invention to select the internal diameter of the outlet passage 52 in order to create sufficient back pressure to facilitate uniform flow throughout the extraction layer 14. Typically D_E is 1 to 3 mm, for a D_C from 5 to 50 mm, where D_E is the internal diameter of the outlet passage 52, and D_C is the internal diameter of the main passage of the container 42.

The apparatus 40 also includes a top retaining ring 53, which has four radially inwardly projecting fingers 54. The retaining ring 53 fits into the container 42 and is held in place by a friction fit, with the fingers 54 holding the top flow distribution 16a in place.

Although the present invention has been described in considerable detail with reference to certain preferred versions thereof, other versions are possible. For example, the apparatus 10 is not limited to use with biological fluids, but can be used, for example, for testing ground water, drinking water, and other liquids for contaminants.

In addition, the extraction media does not have to be homogenous, but rather a different extraction media can be used in a single bed, or the apparatus can include multiple beds of extraction media for extracting different analytes from samples.

Therefore, the spirit and scope of the appended claims should not be limited to the description of the preferred versions contained herein.